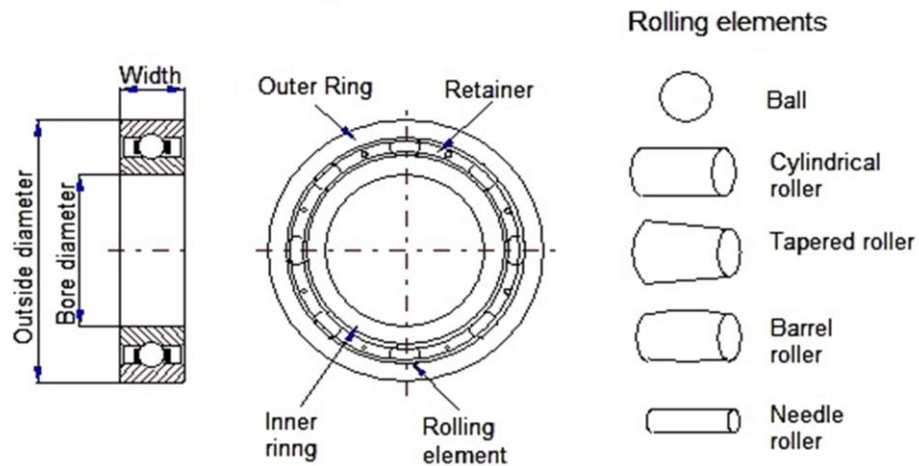


LECTURES FOURTEEN & FIFTEEN**ROLLING CONTACT BEARINGS****Ball and Roller Bearings**

Reference: "Machine Elements in Mechanical Design" 4th Edition in SI units,
By: Robert L. Mott, Chapter 14.

Introduction:

- See all sections on this chapter i.e.

14-1 Objectives of this chapter (Page 600)

14-2 Types of rolling contact bearings (Page 600 to 604)

- See also tables and figures on this chapter.
- See the CD for MDesign which give all types of rolling contact bearings, fixation, and calculations.

Summary of design procedure for rolling contact bearings:

1. From analysis of forces on shaft take reaction on bearing and speed.
2. Specify equivalent load (P) as below:

$$P = VR \quad \dots\dots\dots (14-5) \quad \text{for radial load only (see page 613)}$$

$$P = VXR + YT \quad \dots\dots\dots (14-6) \quad \text{for axial \& radial load (see page 614)}$$

$$\left. \begin{array}{l} P_A = 0.4F_{rA} + 0.5\left(\frac{Y_A}{Y_B}\right) F_{rB} + Y_A T_A \\ P_B = F_{rB} \end{array} \right\} \begin{array}{l} (14-8) \text{ for tapered rolling bearing} \\ \text{(See page 618)} \end{array}$$

Where:

V: Rotation parameter (V=1 if inner race rotating; V=1.2 if outer race rotating)
 R: Radial load; T: Thrust load; X: Radial factor = 0.56;
 Y: Thrust factor (see table 14.5)

Note: for small thrust load X=1 & Y=0 as in equation (14-5)

P_A : Equivalent radial load on bearing A

P_B : Equivalent radial load on bearing B

F_{rA} : Applied radial load on bearing A

F_{rB} : Applied radial load on bearing B

T_A : Thrust load on bearing A

Y_A : Thrust factor for bearing A (from table 14.7 page 614)

Y_B : Thrust factor for bearing B (from table 14.7 page 614)

3. Assume recommended life from table 14-4 (page 612) and find suitable capacity & bearing or choose the bearing then find its life.

$$C = P_d \frac{F_L}{F_n} \quad \text{..... (14-4) page 612}$$

Where:

C: Dynamic load rating

You can also use the following equation for C:

load (P) & life (L) relationship

$$\frac{L_2}{L_1} = \left(\frac{P_1}{P_2}\right)^K \quad \text{.....} \quad (14-1)$$

$$C = P_1 / (L_d / 10^6)^{1/K} \quad (14-3)$$

F_L : Life factor..... see figure (14-12)

F_n : Speed factor see figure (14-12)

K: factor (K=3 for ball bearing & K=3.33 for roller bearing)

$L_2 = L_d$ = Design life at design load ($P_2 = P_d$)

$L_1 = L_{10}$ = Life at load C ($L_{10} = 10^6$ revolution at $P_1 = C$)

$L_2 = L_d$ = (hours) (rpm) (60 min/hr)

Ex: 14-1 (Page 611), Ref. 1:

A catalog lists the basic dynamic load rating for a ball bearing to be (31358 N) for a rated life of 1 million rev. What would be the expected L_{10} life of the bearing if it were subjected to a load of 15568 N)?

Sol:

$P_1 = C = 31358 \text{ N}$; $P_2 = P_d = 15568 \text{ N}$; $L_1 = L_{10} = 10^6 \text{ rev.}$; $K=3$

Find: L_2 = design life at design load P_2

$L_2 = L_d = L_1 (P_1 / P_2)^K = 10^6 (31356 / 15568)^3 = 8.17 * 10^6 \text{ rev.}$

$L_2 = 8.17 * 10^6 \text{ rev. at } P_d = 15568 \text{ N}$

Ex: 14-2 (Page 611), Ref. 1:

Compute the required basic dynamic load rating, C for a ball bearing to carry a radial load of (2891.2 N) from a shaft rotating at 600 rpm that is part of an assembly conveyor in a manufacturing plant.

Sol:

$C = ?$; $P_d = 2891.2 \text{ N}$; $n = 600 \text{ rpm}$; Application: conveyor

From eq.(14-3) $C = P_d (L_d / 10^6)^{1/K}$ $K=3$

$$L_d = \{30000 \text{ hr (from table 14-4, page 612)}\} * 600 \text{ rpm} * (60 \text{ min/hr})$$

$$L_d = 1.08 * 10^9 \text{ rev.}$$

$$C = 2891.2 (1.08 * 10^9 / 10^6)^{1/3} = 29668 \text{ N}$$

Or, you can solve this example as follows:

From figure 14-12 page 612:

$$F_n = 0.381 \text{ at } 600 \text{ rpm (62.82 rad/sec)}$$

$$F_L = 3.9 \text{ at } 30000 \text{ hr life}$$

$$C = P_d (F_L / F_n) \dots \text{Equation (14-4)}$$

$$C = 2891 (3.9 / 0.381) = 29596 \text{ N}$$

Ex: 14-3 (Page 614), Ref.1:

Select a single-row, deep-groove ball bearing to carry (2891 N) of pure radial load from a shaft that rotates at 600 rpm. The design life is to be 30 000 h. The bearing is to be mounted on a shaft with a minimum acceptable diameter of 40 mm.

Sol:

$$R = 2891 \text{ N}; \quad N = 62.82 \text{ rad/sec} = 600 \text{ rpm}; \quad \text{life} = 30000 \text{ hr}; \quad d = 40 \text{ mm}$$

Select a single-row deep groove ball bearing

$V = 1$ for inner race rotating

Use table 14-3 page 607 to page 609 at $d = 40 \text{ mm}$; choose:

A-series 6200 \longrightarrow $C = 22.46 \text{ KN}$ at $d = 40 \text{ mm}$ type 6208

B-series 6300 \longrightarrow $C = 31.36 \text{ KN}$ at $d = 40 \text{ mm}$ type 6308

But from Ex: 14-2 (page 611) choose type 6308, $C = 31.36 \text{ KN}$

Which is greater than 29.7 KN?

Ex: 14-4 (Page 615), Ref.1:

Select a single-row, deep-groove ball bearing from Table 14-3 to carry a radial load of (8220 N) and a thrust load of (3002 N). The shaft is to rotate at 1150 rpm, and a design life of 20 000 h is desired. The minimum acceptable diameter for the shaft is 78.74 mm.

Sol:

$$R = 8228 \text{ N}; \quad T = 3002 \text{ N}; \quad N = 120.4 \text{ rad/sec}; \quad L_d = 20000 \text{ hr}; \quad d \geq 78.74 \text{ mm}$$

Select a single-row deep groove ball bearing?

$$P = VXR + YT \dots \dots \dots (14-6)$$

$$\text{Assume } Y = 1.5; \quad V = 1 \text{ (inner race rotates)}; \quad X = 0.56$$

$$P = (1 \times 0.56 \times 8228) + (1.5 \times 3002) = 9113 \text{ N}$$

$$F_n = 0.3 \text{ \& } F_L = 3.41 \longrightarrow C = P \cdot F_L / F_n = 9113 \times 3.41 / 0.3 = 103.64 \text{ KN} = 23300 \text{ lb}$$

From table 14-3 \longrightarrow choose 6222 or 6318, so take 6318 with $d = 90 \text{ mm}$,

So at this bearing the following information are:

Bearing No.	d	D	B	C ₀	C
6318	90 mm	190 mm	43 mm	100.1 KN	109.8 KN

Now we should check the suitable Y and we will make the new calculation:

$$T/C_0 = 3002/100100 = 0.03 \text{ \& from table 14-5 (Page 614) } \longrightarrow Y = 1.97$$

$$P = VXR + YT = (1 \times 0.56 \times 8228) + (1.97 \times 3002) = 10523 \text{ N}$$

$$\text{\& } C = 10523 (3.41/0.3) = 119651 \text{ N} = 119.6 \text{ KN} = 29700 \text{ lb}$$

(from table 14-3), $119.6 \text{ KN} (29700 \text{ lb}) < 133.44 \text{ KN} (30000 \text{ lb})$

This bearing is satisfactory.

Bearing No.	d	D	B	C ₀	C
6320	100 mm	215 mm	47 mm	132.6 KN	133.4 KN

Ex: 14-5 (Page 619), Ref.1:

The shaft shown in Figure 14-15 carries a transverse load of (30246 N) and a thrust load of (11120 N). The thrust is resisted by bearing A. The shaft rotates at 350 rpm and is to be used in a piece of agricultural equipment. Specify suitable tapered roller bearings for the shaft.

Sol:

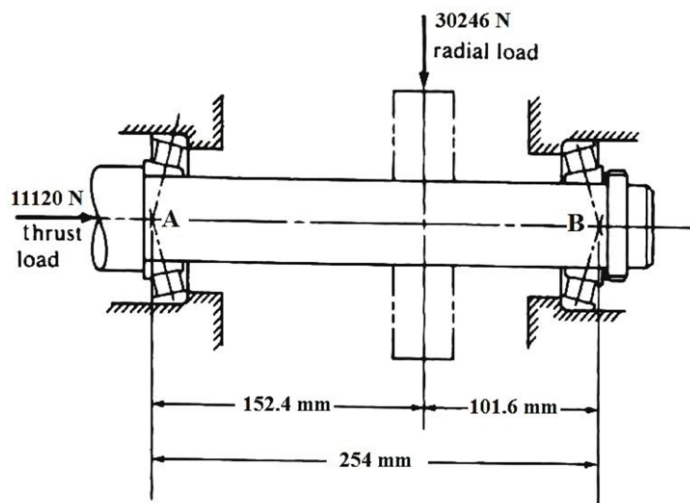
The thrust resisted by bearing A

$$N = 36.64 \text{ rad/sec}$$

Application:

Agricultural Equipment

Select suitable tapered rolling bearing contact for shaft?



$$F_{rA} = 30246 \times (101.6/254) = 1209$$

$$F_{rB} = 30246 \times (152.4/254) = 18147 \text{ N}$$

$$T_A = 11120 \text{ N}$$

Assume $Y_A = Y_B = 1.75$

Now use equation 14-8 $\longrightarrow P_A = 0.4F_{rA} + 0.5 \frac{Y_A}{Y_B} F_{rB} + Y_A T_A$

$$P_A = 0.4 (12098) + 0.5(1.75/1.75) (18147) + 1.75 (11120) = 33373 \text{ N}$$

$$P_B = F_{rB} = 18147 \text{ N}$$

From table 14-4 \longrightarrow choose $L_d = 4000h * (350 \text{ rpm}) * 60 \text{ min/h}$

$$L_d = 8.4 * 10^7 \text{ rev.}$$

From eq. 14-3 $\longrightarrow C_A = P_A (L_d/10^6)^{1/K} = 33373 (8.4*10^7/10^6)^{1/3.33}$

$$C_A = 126323 \text{ N} = 28400 \text{ lb}$$

$$\& C_B = P_B (L_d/10^6)^{1/K} = 18147 (8.4*10^7/10^6)^{1/3.33} = 68499 \text{ N} = 15400 \text{ lb}$$

From table 14-7 (page 619) \longrightarrow choose the following bearings:

Bearing A $\longrightarrow d = 63.5 \text{ mm}$; $D = 127 \text{ mm}$; $Y_A = 1.65$; $C = 130326 \text{ N}$

Bearing B $\longrightarrow d = 44.45 \text{ mm}$; $D = 106.6 \text{ mm}$; $Y_B = 1.5$; $C = 95187 \text{ N}$

Now we should check our calculation as follows:

$$P_A = 0.4(12098) + 0.5(1.65/1.5) (18147) + 1.65 (11120) = 33168 \text{ N}$$

$$\& P_B = F_{rB} = 18147 \text{ N}$$

$$C_A = 125433 \text{ N} \quad \& \quad C_B = 68499 \text{ N}$$

They are still satisfactory for the selected bearings.

Note: if $P_A < F_{rA}$ then let $P_A = F_{rA}$ and compute P_B

$$P_B = 0.4 F_{rB} + 0.5 (Y_B/Y_A) (F_{rA}) - (Y_B T_A) \quad \text{..... 14-10 (Page 620)}$$

Note: follow the same procedure for Angular contact ball bearing.

7-3: Life predication under varying loads, (Page 625):

$$\text{Mean effective load } (F_m) = \left\{ \frac{\sum i (F_i)^P N_i}{N} \right\}^{\frac{1}{P}}$$

Where: F_i = individual load among a series of i loads

N_i = No. of revolutions at which F_i operates

N = total No. of revolutions in complete cycle

$P = 3$ for ball bearings; $P = 10/3$ for roller bearings

N_i = No. of minutes of operation at F_i

N = the sum of no. of minutes in the total cycle = $N_1 + N_2 + \dots + N_i$

Expected life in millions of revolutions is:

$$L = (C/F_m)^P \quad \dots\dots\dots 14-12$$

Ex: 14-6 (Page 626), Ref.1:

A single-row, deep-groove ball bearing number 6308 is subjected to the following set of loads for the given times

Condition	F_i	Time
1	2891 N	30 min.
2	3336 N	10 min.
3	1112 N	20 min.

This cycle of 60 min is repeated continuously throughout the life of the bearing. The shaft carried by the bearing rotates at 600 rpm (62.82 rad/sec). Estimate the total life of the bearing.

Sol:

$$F_m = \left\{ \frac{\sum i (F_i)^P N_i}{N} \right\}^{\frac{1}{P}}$$

$$= \left\{ \frac{30 (2891)^3 + 10 (3336)^3 + 20 (1112)^3}{30+10+20} \right\}^{1/3} = 2655 \text{ N}$$

$$L = (C/F_m)^P = \{(31358 \text{ (tab. 14-3 for No. 6308)}) / 2655\}^3 = 1647 \text{ million rev.}$$

$$L = (1647 \times 10^6 / 1) * (\text{min} / 600 \text{ rev.}) * (\text{h} / 60 \text{ min.}) = 4574 \text{ hours}$$